Funnel control

Origin and recent advances

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Who am I?

Stephan Trenn

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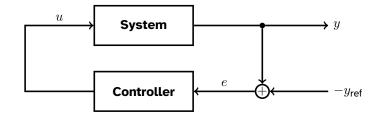
Associate Professor for Systems & Control, Bernoulli Institute **Programme Director** for master degrees Math., Applied Math., Systems & Control

- > studied Mathematics and Computer Science in Ilmenau, Germany
- six month Erasmus student in Southampton, UK
- > PhD 2009 in mathematical control theory in Ilmenau
- Postdoc (9 month) at University of Illinois, Urbana-Champaign, USA
- Postdoc (17 month) at University of Würzburg, Germany
- > Assistant Professor for Math. Control Theory (2011 2017), Kaiserslautern, Germany

Research:

- Switched systems
- > Differential-algebraic equations (DAEs)
- > Funnel control

Control Task

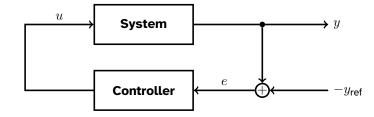


Goal: Output tracking $y(t) \approx y_{\text{ref}}(t)$

Applications

- Flying to the moon
- > Robotics
- > (Adaptive) cruise control in cars
- Chemical processes

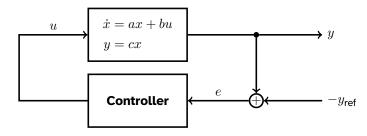
Introduction



Goal: Output tracking $y(t) \approx y_{\rm ref}(t)$

Challenge

- no exact knowledge of system model
- > no future knowledge or model for reference signal

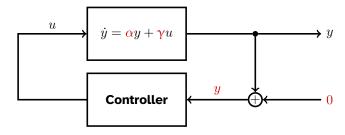


Assumptions

- > Known model structure
- \rightarrow Known sign of high frequency gain $\gamma := cb$, assume $\gamma > 0$
- $y_{ref} = 0$

Introduction

Unknown system parameters α and γ



Goal

Introduction

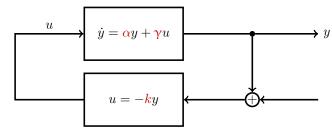
Design output feedback u such that $y(t) \to 0$ as $t \to \infty$

If we would know α, γ , how would we choose u?

Goal: $\dot{y} \stackrel{!}{=} -\lambda y \quad \Rightarrow \quad \text{achievable with } u = -ky \text{ and } k := \frac{\alpha + \lambda}{\gamma}$

In general, with u = -ky we have $\dot{y} = (\alpha - \gamma k)y$

The scalar linear case with $y_{ref} = 0$



Hence we have arrived at our first high gain control result:

Theorem

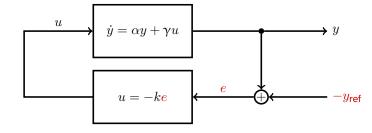
The proportional negative feedback

$$u = -ky$$

achieves convergence for all $k > \frac{\alpha}{\gamma}$.

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What happens for $y_{ref} \neq 0$?



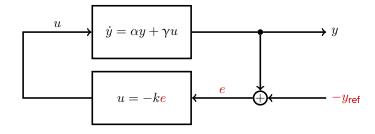
Error dynamics: $\dot{e} = \dots = (\alpha - \gamma k)e + \alpha y_{ref} - \dot{y}_{ref}$

Equilibrium for constant y_{ref} :

$$0 = (\alpha - \gamma k)e + \alpha y_{\text{ref}} \quad \Longleftrightarrow \quad e = \frac{\alpha}{\gamma k - \alpha} y_{\text{ref}} \neq 0$$

→ no convergence to zero anymore

What happens for $y_{ref} \neq 0$?



In general: Practical tracking with high gain control:

Theorem

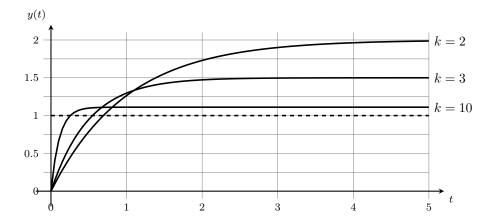
Introduction

If y_{ref} and \dot{y}_{ref} are bounded, then

$$\forall y_0 \ \forall \varepsilon > 0 \ \exists K_{\varepsilon} > 0 \ \forall k > K_{\varepsilon} \ \exists T_{k,\varepsilon,y_0} > 0 : \quad |e(t)| < \varepsilon \quad \forall t \geq T_{k,\varepsilon,y_0}$$

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Example $\alpha = 1$, $\gamma = 1$, $y_{\text{ref}} \equiv 1$





Introduction

High gain for relative degree one systems

Relative degree and zero dynamics High gain stabilization Nonlinear systems

Adaptive choice of gain

Adaptive stabilization λ -tracking

The funnel controller

The original funnel controller with proof sketch Relative degree two funnel controller Bang-bang funnel control Funnel synchronization

Summary

Relative degree

$$\dot{x} = Ax + bu$$

$$y = cx$$

$$A \in \mathbb{R}^{n \times n}, b, c^{\top} \in \mathbb{R}^{n}$$
(*)

Definition (Relative degree)

Write
$$g(s) := c(sI - A)^{-1}b$$
 as $g(s) = \frac{p(s)}{g(s)}$.

Then $r := \deg q(s) - \deg p(s)$ is called relative degree of (*).

Remarks:

- For $p(s) \not\equiv 0$: $0 \le \deg p(s) < \deg q(s) \le n \quad \rightsquigarrow \quad r \in \{1, 2, \dots, n\}$.
- $if q(s) = 0 = p(s); r = \infty$
- If (*) has feedthrough term, i.e. y = cx + du with $d \neq 0$, then r := 0
- > For descriptor systems the relative degree can also be negative



Relative degree and Markov parameters

$$\dot{x} = Ax + bu
 y = cx$$

$$A \in \mathbb{R}^{n \times n}, b, c^{\top} \in \mathbb{R}^{n}$$
(*)

Definition (Markov parameters)

The numbers $M_k := cA^kb$, $k \in \mathbb{N}$, are called Markov parameters of (*).

Lemma (Transfer function and Markov parameters)

$$g(s) = c(sI - A)^{-1}b = c\sum_{k=0}^{\infty} \frac{A^k}{s^{k+1}}b = \sum_{k=0}^{\infty} \frac{M_k}{s^{k+1}}$$

Lemma (Markov parameters and relative degree)

$$r = \min \{ k \in \mathbb{N}_{>0} \mid M_{k-1} \neq 0 \}$$

Intuition for relative degree

$$\begin{aligned} \dot{x} &= Ax + bu \\ y &= cx + du \end{aligned} \qquad A \in \mathbb{R}^{n \times n}, b, c^{\top} \in \mathbb{R}^{n}$$
 (*)

 $d \neq 0 \iff \text{r.d. } 0$

 \rightarrow input u directly influences y = cx + du

d=0 and $cb \neq 0 \iff \text{r.d. } 1$

 $\rightarrow y$ not directly influenced by u, but $\dot{y} = c\dot{x} = cAx + cbu$ directly influenced by u

d=0, cb=0 and $cAb \neq 0 \iff$ r.d. 2

ightharpoonup y, \dot{y} not directly influence by u, but $\ddot{y}=cA\dot{x}=cA^2x+cAbu$ directly influenced by u

:

 $d=0,\,cb=0,\,\ldots,\,cA^{r-2}b=0$ and $cA^{r-1}b\neq 0\iff r.d.\,r$ $y,\ldots,y^{(r-1)}$ not influenced by u, but $y^{(r)}=cA^rx+cA^{r-1}b\,u$ directly influence by u

Intuition behind relative degree

Relative degree = lowest derivative of y which is directly influence by input u



Zero dynamics

Zero dynamics

Question

What input is needed to keep the output identically zero?

Relative degree
$$r \in \{1,2,\dots,n\}$$
 $\qquad 0 \stackrel{!}{=} y^{(r)}(t) = cA^rx(t) + \underbrace{cA^{r-1}b}_{=:\gamma}u(t) \; \forall t$ $\qquad \qquad u(t) = -\frac{1}{\gamma}cA^rx(t) \; \text{keeps output identically zero}$ $\qquad \qquad \dot{x} = (A - \frac{1}{\gamma}bcA^r)x \; \text{is called zero dynamics}^1 \; \text{(ZD)}$

Problem

Unstable ZD \rightarrow unbounded state x

→ unbounded input needed to keep output bounded

¹when considered on the subspace $\ker[c/cA/\dots/cA^{r-1}]$, which results from the conditions $0=y^{(k)}(t)=cA^kx(t)$, $k=0,1,\dots,r-1$, i.e. $x(t)\in\ker[c/cA/\dots/cA^{r-1}]$

Stable zero dynamics

Theorem

(*) has stable ZD
$$\iff$$
 rank $\begin{bmatrix} \lambda I - A & b \\ c & 0 \end{bmatrix} = n + 1$ for all $\lambda \in \mathbb{C}_{\text{Re} \geq 0}$.

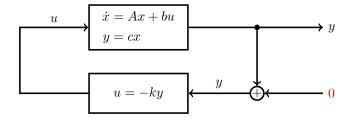
If (*) is controllable and observable, then it has stable ZD $\iff p(s)$ is stable

Remarks

- The property of having stable ZD is related to the notion minimum phase²: $|g_1(i\omega)| = |g_2(i\omega)|$ and the first has stable ZD $\implies \arg g_1(i\omega) \le \arg g_2(i\omega)$
- if (*) is stabilizable, unstable ZD can be stabilized by state feedback, but not by (static) output feedback
- > Stable ZD implies stabilizability and detectability, but not the other way around in general

²For more on minimum phase see: Ilchmann, A., Wirth, F. (2013). On minimum phase. at-Automatisierungstechnik, 61(12), 805-817.

High gain stabilization for r.d.-one systems

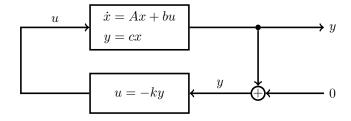


Assumptions:

> Relative degree $r=1 \Leftrightarrow \gamma := cb \neq 0$, in particular:

- \rightarrow positive high frequency gain $\Leftrightarrow \gamma > 0$
- \rightarrow stable zero-dynamics (minimum phase) \Leftrightarrow A_{22} Hurwitz

High gain stabilization for r.d.-one systems

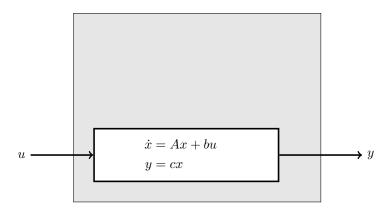


Theorem (High-gain stabilization)

cb>0 and stable zero-dynamics

$$\Rightarrow \exists K > 0 \ \forall \ k \geq K$$
: Closed loop is asymptotically stable

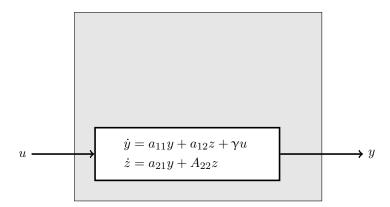
Key idea of proof: Show that $\begin{bmatrix} a_{11} - \gamma k & a_{12} \\ a_{21} & A_{22} \end{bmatrix}$ is Hurwitz for sufficiently large k.



Adaptive choice of gain

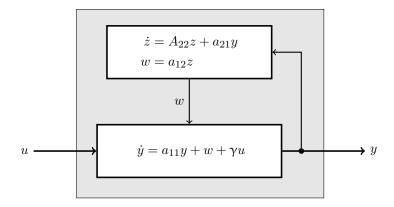
Introduction

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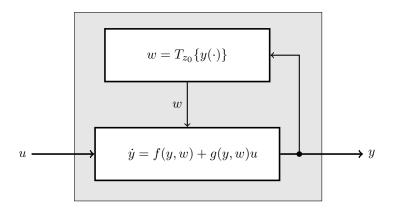


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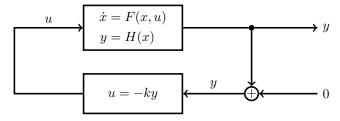




Assumptions:

- T_{z_0} is causal BIBO operator, i.e. $\exists \kappa(\cdot): \|w\| \leq \kappa(\|y\|)$
- \rightarrow f and g continuous and g > 0

High gain stabilization for nonlinear systems



Theorem

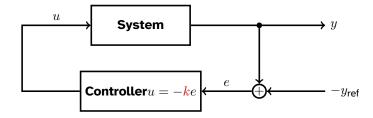
Assume there exists (nonlinear) coordinate transformation such that system is equivalent to

$$\dot{y} = f(y, w) + g(y, w)u, \quad w = T_{z_0}\{y(\cdot)\}\$$

with f, g continuous, T_{z_0} causal BIBO operator and g > 0, then

$$\forall y_0 \ \forall \eta_0 \ \forall \varepsilon > 0 \ \exists K > 0 \ \forall k \geq K \ \exists T > 0 : \quad |e(t)| < \varepsilon \quad \forall t \geq T$$

Summary high gain feedback



Goal: Output tracking

Challenge: Unknown system parameters

Structural assumptions

- Relative degree one with known sign of "high frequency gain"
- Stable zero dynamics

High gain feedback: u = -ke "works" for sufficiently large gain k > 0

Remaining challenge: When is k sufficiently large?



Introduction

Introduction

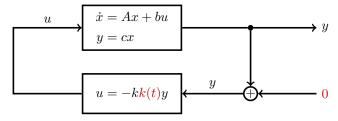
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Adaptive stabilization λ -tracking

The funnel controller

Summary



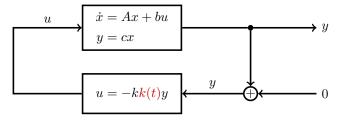
Theorem (High-gain stabilization)

$$cb > 0$$
 and stable zero-dynamics $\Rightarrow \exists K > 0 \ \forall \ k \geq K : y(t) \rightarrow 0$

Key idea

Why not make k time-varying with $\dot{k}(t) > 0$ as long as y(t) > 0?

Choosing gain adaptively, linear case



Theorem (Adaptive High-Gain Feedback, Byrnes & Willems 1984)

cb>0 and stable zero-dynamics \Rightarrow

$$\dot{k}(t) = y(t)^2$$
 makes closed loop asymptotically stable

and $k(\cdot)$ remains bounded

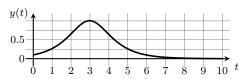
Boundedness of $k(t) = \int_0^t y(s)^2 ds$ follows from final exponential decay of y.

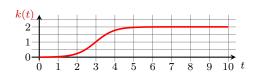
Simulations

Introduction

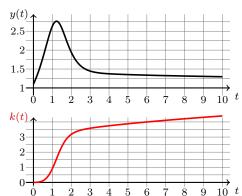
$$\dot{y} = y + u, \quad u(t) = -k(t)(y(t) - y_{\mathsf{ref}}(t)), \quad \dot{k} = (y - y_{\mathsf{ref}})^2$$

output and gain for $y_{\mathsf{ref}} = 0$

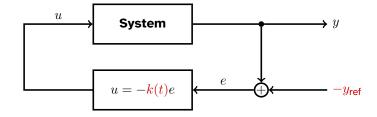




output and gain for $y_{ref} = 1$



High gain adaptive control and tracking?

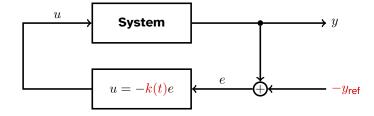


Unbounded gain

For $y_{\text{ref}} \neq 0$ the adaptation rule $\dot{k} = e^2$ leads to unbounded gain.

Recall: Constant gain for $y_{\text{ref}} \neq 0$ only leads to practical tracking, i.e. $e(t) \not\to 0$

High gain adaptive control and tracking?

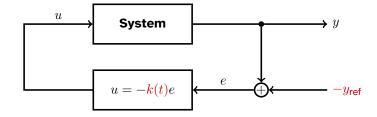


How to prevent unbounded growth?

Stop increasing gain when error is sufficiently small, e.g. via

$$\dot{k}(t) = \begin{cases} 0 & |e(t)| \le \lambda \\ |e(t)|(|e(t)| - \lambda) & |e(t)| > \lambda \end{cases}$$

High gain adaptive control and tracking?



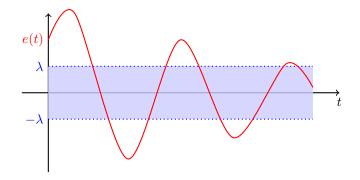
Theorem (λ -tracking, Ilchmann & Ryan 1994)

Assume r.d.-one with " $\gamma > 0$ ", stable zero-dynamics and $y_{\rm ref}, \dot{y}_{\rm ref}$ bounded. For $\lambda > 0$ consider

$$\dot{k}(t) = \begin{cases} 0, & |e(t)| \le \lambda, \\ |e(t)| (|e(t)| - \lambda), & |e(t)| > \lambda. \end{cases}$$

Then the closed loop is practically stable, i.e. $\limsup_{t\to\infty} |e(t)| \leq \lambda$.

Remaining problems of λ -tracker



Problems:

- No guarantees when $|e(t)| \le \lambda$
- > No bounds on transient behaviour
- \rightarrow Monotonically growing $k(\cdot)$ \Rightarrow Measurement noise unnecessarily amplified



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Introduction

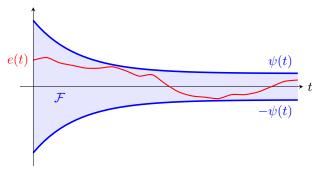
High gain for relative degree one systems

Adaptive choice of gain

The funnel controller

The original funnel controller with proof sketch Relative degree two funnel controller Bang-bang funnel control Funnel synchronization

Summary



$$\mathcal{F} = \mathcal{F}(\psi) := \{(t, e) \mid |e| < \psi(t)\}$$

Idea: k(t) large

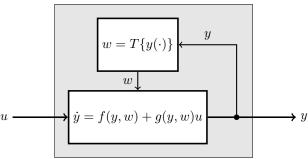
 \iff

Distance of e(t) to funnel boundary small

 \sim Funnel gain:

 $k(t) = \frac{1}{\psi(t) - |e(t)|}$

Funnel controller works



System class

Equivalent to structure left:

- \rightarrow T is causal and BIBO
- \rightarrow f, g continuous
- g > 0

Theorem (Ilchmann, Ryan, Sangwin 2002)

Assume $y_{\text{ref}}, \dot{y}_{\text{ref}}, \psi, \dot{\psi}$ bounded, $\liminf_{t \to \infty} \psi(t) > 0$ and $|e(0)| < \psi(0)$ where $e := y - y_{\text{ref}}$. Then

$$u(t) = -k(t)e(t)$$
 with $k(t) = \frac{1}{\psi(t) - |e(t)|}$

ensures that e(t) remains within funnel $\mathcal{F}(\psi)$ while k(t) remains bounded.

Proof

Step 1: Existence of solution

- Standard ODE theory: solution of closed loop exists on $[0,\omega)$ for $\omega \in (0,\infty]$
- Choose $\omega > 0$ maximal
- If $\omega < \infty$ then " $|e(\omega)| = \psi(\omega)$ "

Step 2: We show that $\omega < \infty$ implies $|e(t)| - \psi(t) > \varepsilon$ for some $\varepsilon > 0$ Error dynamics are given by

$$\dot{e} = f(y, w) - \dot{y}_{ref} + g(y, w)u$$

Step 2a: Boundedness of e, y, and w

e(t) within funnel for $t \in [0, \omega)$

(domain of ODE)

 $\Rightarrow e$ bounded on $[0,\omega)$

(because ψ is bounded)

 $\Rightarrow y$ bounded on $[0,\omega)$

(because y_{ref} is bounded)

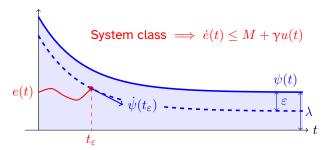
 $\Rightarrow w$ bounded on $[0,\omega)$

(because T is BIBO) (continuity)

 $\Rightarrow f(y,w)$ bounded and g(y,w) bounded away from zero on $[0,\omega)$

 $\Rightarrow \dot{e}(t) < M + \gamma u(t)$ if u(t) < 0 and $\dot{e}(t) > -M + \gamma u(t)$ if u(t) > 0

Step 2b: Funnel invariant (case e(t) > 0)



$$\text{Assumptions: } \varepsilon < \psi(0) - e(0) \qquad \quad \varepsilon < \lambda/2 \qquad \quad \psi(t) \geq \lambda$$

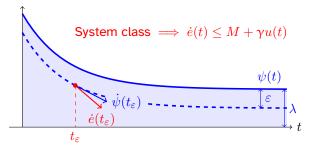
$$\psi(t) \ge 1$$

$$e(t_{\varepsilon}) = \psi(t_{\varepsilon}) - \varepsilon \implies k(t_{\varepsilon}) = \frac{1}{\psi(t_{\varepsilon}) - |e(t_{\varepsilon})|} = \frac{1}{\varepsilon}$$

$$\implies u(t_{\varepsilon}) = -k(t_{\varepsilon})e(t_{\varepsilon}) \le -\frac{1}{\varepsilon}\frac{\lambda}{2}$$

$$\implies \dot{e}(t_{\varepsilon}) \le M - \frac{\gamma\lambda}{2\varepsilon}$$

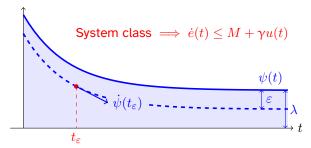
Step 2b: Funnel invariant (case e(t) > 0)



Assume
$$\dot{\psi}(t) > -\Psi$$
 and $\varepsilon \leq \frac{\gamma \lambda}{2(\Psi + M)}$ we have

$$\dot{e}(t_{arepsilon}) \leq M - rac{\gamma \lambda}{2arepsilon} \leq -\Psi < \dot{\psi}(t_{arepsilon})$$

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Consequence: For sufficiently small $\varepsilon > 0$,

$$\mathcal{F}_{\varepsilon} := \{ (t, e) \mid |e(t)| < \psi(t) - \varepsilon \}$$

is positively invariant, i.e.

$$(0, e(0)) \in \mathcal{F}_{\varepsilon} \quad \Rightarrow \quad (t, e(t)) \in \mathcal{F}_{\varepsilon} \ \forall t \ge 0$$

and $\omega < \infty$ impossible!

Extensions of funnel controller

- Asymptotic tracking (Lee & Trenn 2019)
- > Multi-Input Multi-Output (MIMO) (already in Ilchmann et al. 2002)
- > Higher relative degree (Ilchmann et al. 2007, Berger et al. 2018)
- > Input saturation (Ilchmann et al. 2004, Hopfe et al. 2010)
- Bang-Bang funnel control (Liberzon & Trenn 2013)
- > Funnel synchronization for multi-agent systems (Shim & Trenn 2015)
- For DAE-systems (Berger 2016)
- For impulsive systems (Karimi Pour & Trenn 2025)

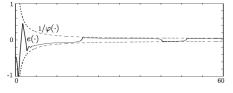
Relative degree two via backstepping

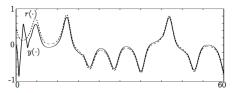
For rel. deg. two systems, Funnel Controller is given by (Ilchmann et al. 2007):

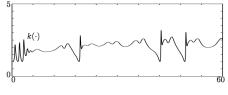
$$u(t) = -k(t)e(t) - (\|e(t)\|^2 + k(t)^2)k(t)^4(1 + \|\xi(t)\|^2)(\xi(t) + k(t)e(t))$$

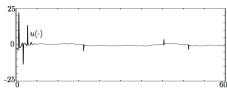
$$k(t) = 1/(1 - \varphi(t)^2 \|e(t)\|^2)$$

$$\dot{\xi}(t) = -\xi(t) + u(t)$$









Alternative Approach for relative degree two

Use two funnels, one for error and one for derivative of error

Simple Control Law

$$u(t) = -k_0(t)^2 e(t) - k_1(t)\dot{e}(t)$$

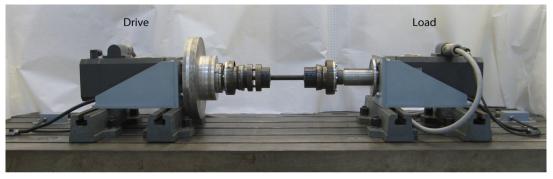
$$k_i(t) = \frac{1}{\psi_i(t) - |e^{(i)}(t)|}, \quad i = 0, 1$$

System class:
$$\ddot{y}(t) = f(p_f(t), T_f\{y, \dot{y}\}(t)) + g(p_g(t), T_g\{y, \dot{y}\}(t))u(t)$$

Theorem (Hackl et al. 2012)

The above Funnel Controller for relative-degree-two-systems works (under mild assumptions on ψ_0 and ψ_1).

Experimental verification



$$\dot{x}(t) = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} x(t) + \begin{bmatrix} 0 \\ \gamma \end{bmatrix} (u(t) + u_L(t) - (Tx_2)(t)),$$

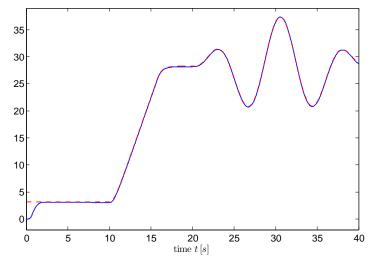
$$y(t) = \begin{bmatrix} 1 & 0 \end{bmatrix} x(t),$$

 x_1 : angle of rotating machine, $x_2 = \dot{x}_1$: angular velocity

 u_L : unknown (bounded) load

 $T: \mathbb{C}(\mathbb{R}_{\geq 0} \to \mathbb{R}) \to \mathbb{L}^{\infty}_{loc}(\mathbb{R}_{\geq 0} \to \mathbb{R})$ friction operator

Tracking control in experiment

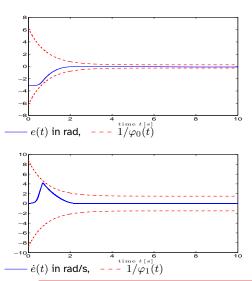


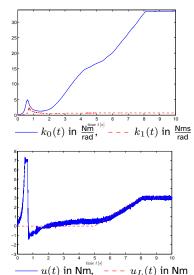
Measured angle y(t) in rad, --- reference angle $y_{ref}(t)$ in rad



Introduction

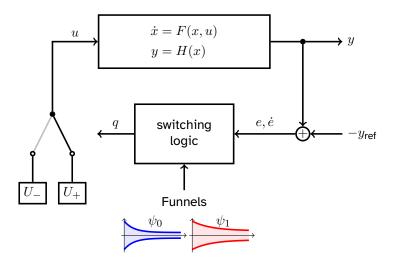
Experiment: Error, gains, input





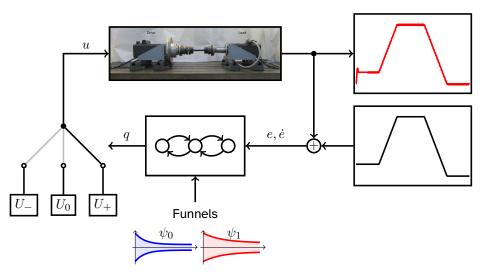
Introduction

Bang-Bang Funnel Control



Introduction

Bang-Bang Funnel Control



Funnel synchronization - setup

Given

 \rightarrow N agents with individual n-dimensional dynamics:

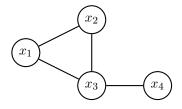
$$\dot{x}_i = f_i(t, x_i) + u_i$$

- \rightarrow undirected connected coupling-graph G = (V, E)
- \rightarrow local feedback $u_i = \gamma_i(x_i, x_{\mathcal{N}_i})$

Desired

Control design for practical synchronization

$$x_1 \approx x_2 \approx \ldots \approx x_n$$



$$u_1 = \gamma_1(x_1, x_2, x_3)$$

$$u_2 = \gamma_2(x_2, x_1, x_3)$$

$$u_3 = \gamma_3(x_3, x_1, x_2, x_4)$$

$$u_4 = \gamma_4(x_4, x_3)$$



A "high-gain" result

Let $\mathcal{N}_i := \{j \in V \mid (j,i) \in E\}$ and $d_i := |\mathcal{N}_i|$ and \mathcal{L} be the Laplacian of G.

Diffusive coupling

$$u_i = -k \sum_{j \in \mathcal{N}_i} (x_i - x_j)$$
 or, equivalently, $u = -k \mathcal{L} x$

Theorem (Practical synchronization, Kim et al. 2013)

Assumptions: G connected, all solutions of average dynamics

$$\dot{s}(t) = \frac{1}{N} \sum_{i=1}^{N} f_i(t, s(t))$$

remain bounded. Then $\forall \varepsilon > 0 \ \exists K > 0 \ \forall k \geq K$: Diffusive coupling results in

$$\limsup_{t \to \infty} |x_i(t) - x_j(t)| < \varepsilon \quad \forall i, j \in V$$

Remarks on high-gain result

Common trajectory

It even holds that

$$\limsup_{t\to\infty} |x_i(t) - s(t)| < \varepsilon/2,$$

where
$$s(\cdot)$$
 solves $\dot{s}(t)=rac{1}{N}\sum_{i=1}^{N}f_i(t,s(t))$, $s(0)=rac{1}{N}\sum_{i=1}^{N}x_i$.

Independent of coupling structure and amplification k.

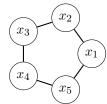
Error feedback

With $e_i:=x_i-\overline{x}_i$ and $\overline{x}_i:=\frac{1}{d_i}\sum_{i\in\mathcal{N}_i}x_j$ diffusive coupling has the form

$$u_i(t) = -ke_i(t)$$

Attention: $e_i \neq x_i - s$, in particular, agents do not know "limit trajectory" $s(\cdot)$

Example (taken from Kim et al. 2015)



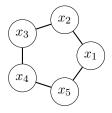
Simulations in the following for ${\cal N}=5$ agents with dynamics

$$f_i(t, x_i) = (-1 + \delta_i)x_i + 10\sin t + 10m_i^1\sin(0.1t + \theta_i^1) + 10m_i^2\sin(10t + \theta_i^2),$$

with randomly chosen parameters $\delta_i, m_i^1, m_i^2 \in \mathbb{R}$ and $\theta_i^1, \theta_i^2 \in [0, 2\pi]$.

Parameters identical in all following simulations, in particular $\delta_2 > 1$, hence agent 2 has unstable dynamics (without coupling).

Example (taken from Kim et al. 2015)



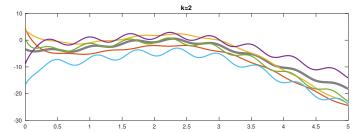
university of

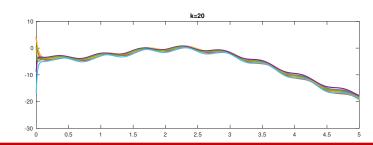
$$u = -k \mathcal{L} x$$

gray curve:

$$\dot{s}(t) = \frac{1}{N} \sum_{i=1}^{N} f_i(t, s(t))$$

$$s(0) = \frac{1}{N} \sum_{i=1}^{N} x_i(0)$$







Funnel synchronization: Initial idea

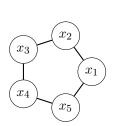
Reminder diffusive coupling: $u_i = -k_i e_i$ with $e_i = x_i - \overline{x}_i$.

Combine diffusive coupling with Funnel Controller

$$u_i(t) = -k_i(t) \, e_i(t)$$
 with $k_i(t) = \frac{1}{\psi(t) - |e_i(t)|}$



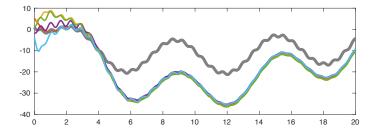
First simulations

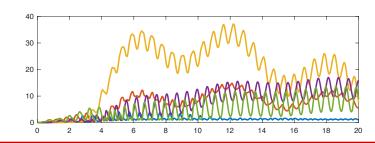


$$u_i(t) = -k_i(t)e_i(t)$$
$$k_i(t) = \frac{1}{\psi(t) - |e_i(t)|}$$

$$\psi(t) = \underline{\psi} + (\overline{\psi} - \underline{\psi})e^{-\lambda t}$$

$$\overline{\psi}=20$$
, $\psi=1$, $\lambda=1$





Observations from simulations

Funnel synchronization seems to work

- > errors remain within funnel
- > practical synchronizations is achieved
- ightarrow limit trajectory does not coincide with solution $s(\cdot)$ of

$$\dot{s}(t) = \frac{1}{N} \sum_{i=1}^{N} f_i(t, s(t)), \qquad s(0) = \frac{1}{N} \sum_{i=1}^{N} x_i(0).$$

What determines the new limiting trajectory?

- Coupling graph?
- > Funnel shape?
- Gain function?

Diffusive coupling revisited

Diffusive coupling for weighted graph

$$u_i = -k \sum_{i=1}^{N} \alpha_{ij} \cdot (x_i - x_j) \longrightarrow u_i = -\sum_{i=1}^{N} k_{ij} \cdot \alpha_{ij} \cdot (x_i - x_j)$$

where $\alpha_{ij} = \alpha_{ji} \in \{0,1\}$ is the weight of edge (i,j)

Conjecture

If $k_{ij} = k_{ji}$ are all sufficiently large, then practical synchronization occurs with desired limit trajectory s of average dynamics.

Proof technique from Kim et al. 2013 should still work in this setup.

Edgewise Funnel synchronization

Diffusive coupling \rightarrow edgewise Funnel synchronization

$$u_i = -\sum_{i=1}^{N} k_{ij} \cdot \alpha_{ij} \cdot (x_i - x_j) \longrightarrow u_i = -\sum_{i=1}^{N} \frac{\mathbf{k}_{ij}(\mathbf{t})}{\mathbf{k}_{ij}} \cdot (x_i - x_j)$$

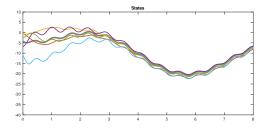
Edgewise error feedback

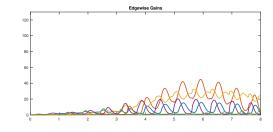
$$k_{ij}(t) = \frac{1}{\psi(t) - |e_{ij}|}, \quad \text{with} \quad e_{ij} := x_i - x_j$$

Properties:

- \rightarrow Decentralized, i.e. u_i only depends on state of neighbors
- \rightarrow Symmetry, $k_{ij} = k_{ji}$
- \rightarrow Laplacian feedback, $u = -\mathcal{L}_K(t, x)x$

Simulation (from Trenn 2017)



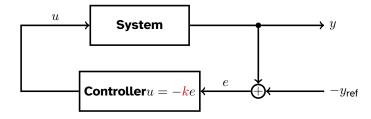


Properties

- + Synchronization occurs
- + Predictable limit trajectory (given by average dynamics)
- + Local feedback law
- + Convergence recently proved (Lee et al. 2023)



Summary high gain feedback and funnel control



Goal: Output tracking

Challenge: Unknown system parameters

Structural assumptions

- Relative degree one with known sign of "high frequency gain"
- > Stable zero dynamics

High gain feedback: u = -ke "works" for sufficiently large gain k > 0

Funnel gain: $k(t) = \frac{1}{\psi(t) - |e(t)|}$ achieves tracking with prescribed perfomance