Instability in Power Systems due to Switching

Stephan Trenn

Jan C. Willems Center for Systems and Control University of Groningen, Netherlands

Joint work with **Tjorben Groß** and **Andreas Wirsen** Fraunhofer ITWM, Kaiserslautern, Germany

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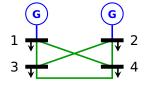
GAMM Annual Meeting 2018, Munich, Germany, 21.03.2018, 17:30



Power systems model

Power grid consists of

- $\rightarrow n_q \in \mathbb{N}$ generators
- > power lines
- $\rightarrow n_a + n_b$ line connectors (**busses**)
- > power demand at each bus



Variables

For each generator:

- $\rightarrow \alpha(t)$ and $\omega(t)$ angle and angular velocity of rotating mass
- $\rightarrow P_a(t)$ generator power acting on turbine For each bus:
- $\rightarrow V(t)$ and $\theta(t)$ voltage modulus and angle
- $\rightarrow P(t)$, Q(t) active and reactive power demand



Basic modelling assumptions

Generator

Modelling

- Rotating mass(es) with linear friction (and linear elastic coupling)
- Constant voltage behind transient reactance model (Kundur 1994)
- \Rightarrow sin($\alpha(t) \theta(t)$) $\approx \alpha(t) \theta(t)$

Busses

- $V(t) \approx 1$ (per unit)
- \Rightarrow sin $(\theta_i \theta_i) \approx \theta_i \theta_i$ for any adjacent busses i and i

Lines

Π-model with negligible conductances

→ reactive power flow can be ignored



Linearized model

Dynamics of *i*-th generator

$$\dot{\alpha}_i(t) = \omega_i(t)$$

$$m_i \dot{\omega}_i(t) = -D_i \omega(t) - P_{e,i}(t) + P_{g,i}(t)$$

where $P_{e,i}(t) = \frac{1}{7}(\alpha_i(t) - \theta_i(t))$ and $m_i > 0$ is the moment of inertia

Linearized power flow balance at each bus i

$$0 = P_i(t) + P_{e,i}(t) - \sum_{i=1}^{n_g + n_b} \ell_{ij}(\theta_i(t) - \theta_j(t)),$$

where $\ell_{ii} = \ell_{ii} \ge 0$ is the line susceptance and $P_{e,i}(t) = 0$ for $i > n_a$

Modelling

Linear DAE model

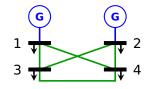
Overall we get a linear DAE

$$E\dot{x} = Ax + Bu$$

where in our example

$$x = (\alpha_1, \alpha_2, \omega_1, \omega_2, \theta_1, \theta_2, \theta_3, \theta_4)^{\top}$$

$$u = (P_{g,1}, P_{g,2}, P_1, P_2, P_3, P_4)^{\top}$$



and, with
$$\ell_{ii} := \sum_{j=1}^{4} \ell_{ij}$$
,

General DAE-structure

DAE-model for n_a generators and n_b busses has the following structure:

$$E\dot{x} = Ax + Bu$$

(powerDAE)

with

Modelling

$$x = (\alpha_1, \dots, \alpha_{n_g}, \omega_1, \dots, \omega_{n_g}, \theta_1, \theta_2, \dots, \theta_{n_g+n_b})^{\mathsf{T}}$$

$$u = (P_{g,1}, \dots, P_{g,n_g}, P_1, \dots, P_{n_g+n_b})^{\mathsf{T}}$$

and

$$E = \begin{bmatrix} I_{n_g} & 0 & 0 \\ 0 & M & 0 \\ 0 & 0 & 0 \end{bmatrix}, \quad A = \begin{bmatrix} 0 & I_{n_g} & 0 \\ -Z^{-1} & -D & \begin{bmatrix} z^{-1} & 0 \\ 0 & 0 \end{bmatrix} \end{bmatrix}, \quad B = \begin{bmatrix} 0 & 0 \\ I_{n_g} & 0 \\ 0 & I_{n_g+n_b} \end{bmatrix}$$

where $\mathfrak{L} = [\ell_{ii}]$ is the (weighted) **Laplacian matrix** of the network



Solvability and Stability

Theorem (Solvability and Stability, *Groß et al. 2016*)

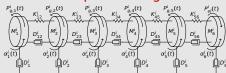
Consider a power grid network and assume that is connected. Then

- (powerDAE) is regular, i.e. existence and uniqueness of solutions
- (powerDAE) has index one, i.e. it is numerically well posed
- (powerDAE) is stable, i.e. all solutions remain bounded

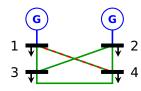
T.B. Gross, S. Trenn, A. Wirsen: Solvability and stability of a power system DAE model, Syst. Control Lett., 29, pp. 12-17, 2016.

Remark

Result remains true for multiple-rotating mass models of generators.



Topological changes



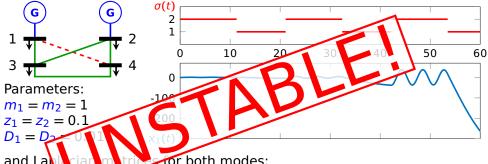
$$E_1\dot{x}=A_1x+B_1u$$
 in mode 1 $E_2\dot{x}=A_2x+B_2u$ in mode 2 or, introducing a switching signal $\sigma:\mathbb{R}\to\{1,2\}$

$$E_{\sigma(t)}\dot{x} = A_{\sigma(t)}x + B_{\sigma(t)}u$$

In fact, topological changes (removal / addition / parameter changes of lines) only effect Laplacian matrix $\mathfrak{L}!$

$$E = \begin{bmatrix} I_{n_g} & 0 & 0 \\ 0 & M & 0 \\ 0 & 0 & 0 \end{bmatrix}, \quad A_{\sigma(t)} = \begin{bmatrix} 0 & I_{n_g} & 0 \\ -Z^{-1} & -D & [Z^{-1} \ 0] \\ [Z^{-1}] & 0 & -\mathcal{L}_{\sigma(t)} - \begin{bmatrix} Z^{-1} \ 0 \end{bmatrix} \end{bmatrix}, \quad B = \begin{bmatrix} 0 & 0 \\ I_{n_g} & 0 \\ 0 & I_{n_g + n_b} \end{bmatrix}$$

Simulation



and La for both modes:

$$\mathfrak{L}_{1} = \begin{bmatrix} 2.01 & 0 & 0.005 & 0.005 \\ \hline 0 & -5.005 & 0.005 & 5 \\ 0.005 & 0.005 & -0.02 & 0.01 \\ 0.005 & 5 & 0.01 & [-5.015] \end{bmatrix}, \quad \mathfrak{L}_{2} = \begin{bmatrix} -2.005 & 0 & 0.005 & 2 \\ \hline 0 & -5.005 & 0.005 & 5 \\ 0.005 & 0.005 & -0.02 & 0.01 \\ 2 & 5 & 0.01 & [-7.01] \end{bmatrix}$$

Instability due to switching

Sufficient condition for stability under arbitrary switching

Stability and Lyapunov functions

$$E_{\sigma}\dot{x} = A_{\sigma}x$$

(swDAE)

Theorem (cf. Liberzon and T. 2012)

Assume (**swDAE**) to be regular and index one. If

- each mode is stable with Lyapunov function $V_p(\cdot)$
- $V_q(\Pi_q x) \leq V_p(x)$ for all p, q and all $x \in \text{im } \Pi_p$ then (swDAE) is stable under arbitrary switching.
- D. Liberzon, S. Trenn: Switched nonlinear differential algebraic equations: Solution theory, Lyapunov functions, and stability. Automatica, 48 (5), pp. 954-963, 2012.

Remark

If E-matrix is switch-independent and has the form $E = \begin{bmatrix} E_1 & 0 \\ 0 & 0 \end{bmatrix}$ with invertible E_1 , then $V_a(\Pi_a x) = V_a(x)$ for all $x \in \text{im } \Pi_p$.



Key lemma

Lemma

Consider (E,A) with structure

$$E = \begin{bmatrix} E_1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}, \quad A = \begin{bmatrix} A_1 & A_2 & 0 \\ A_3 & -\mathfrak{L}_1 + A_4 & -\mathfrak{L}_2 \\ 0 & -\mathfrak{L}_3 & -\mathfrak{L}_4 \end{bmatrix},$$

where $\mathfrak{L} = \begin{bmatrix} \mathfrak{L}_1 & \mathfrak{L}_2 \\ \mathfrak{L}_3 & \mathfrak{L}_4 \end{bmatrix}$ is a (weighted) Laplacian matrix. If

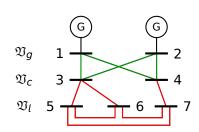
- > (E, A) is regular, index one and stable
- \rightarrow rank $\mathfrak{L}_3 = 1$

then \exists common Lyapunov function for all possible \mathfrak{L}_4

Structural assumption for stability

Assume $\mathfrak{V} = \mathfrak{V}_g \dot{\cup} \mathfrak{V}_c \dot{\cup} \mathfrak{V}_l$ such that

- 1. \mathfrak{V}_g are the generator busses
- 2. no edges between \mathfrak{V}_g and \mathfrak{V}_l
- 3. full connection between \mathfrak{V}_g and \mathfrak{V}_c
- 4. Laplacian of edges between \mathfrak{V}_g and \mathfrak{V}_c has rank one
- 5. topological changes only occur in edges in $\mathfrak{V}_c \cup \mathfrak{V}_l$



Theorem (Groß et al. 2018)

Under above assumptions, stability is preserved under arbitrary switching.

T.B. Gross, S. Trenn, A. Wirsen: Switch induced instabilities for stable power system DAE models. To appear in *Proceedings of IFAC Conference on Analysis and Design of Hybrid Systems (ADHS 2018)*, Oxford, UK, 2018.

Summary

- > Presented a simple linear DAE-model for power grids
- > This DAE model is regular, index 1 and stable
- Sudden repeated changes in line parameter may lead to instability
- Topological conditions are presented which prevent instability

Open questions

- > Physical interpretation
- > Nonlinear and more detailed model