# Instability in Power Systems due to Switching 

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## Power systems model

Power grid consists of
> $n_{g} \in \mathbb{N}$ generators
> power lines
> $n_{g}+n_{b}$ line connectors (busses)
> power demand at each bus


## Variables

For each generator:
> $\alpha(t)$ and $\omega(t)$ angle and angular velocity of rotating mass
> $P_{g}(t)$ generator power acting on turbine
For each bus:
> $V(t)$ and $\theta(t)$ voltage modulus and angle
> $P(t), Q(t)$ active and reactive power demand

## Basic modelling assumptions

## Generator

> Rotating mass(es) with linear friction (and linear elastic coupling)
> Constant voltage behind transient reactance model (Kundur 1994)
$>\sin (\alpha(t)-\theta(t)) \approx \alpha(t)-\theta(t)$

## Busses

, $V(t) \approx 1$ (per unit)
$>\sin \left(\theta_{i}-\theta_{j}\right) \approx \theta_{i}-\theta_{j}$ for any adjacent busses $i$ and $j$

## Lines <br> $\Pi$-model with negligible conductances <br> $\hookrightarrow$ reactive power flow can be ignored

## Linearized model

## Dynamics of $i$-th generator

$$
\begin{aligned}
\dot{\alpha}_{i}(t) & =\omega_{i}(t) \\
m_{i} \dot{\omega}_{i}(t) & =-D_{i} \omega(t)-P_{e, i}(t)+P_{g, i}(t)
\end{aligned}
$$

where $P_{e, i}(t)=\frac{1}{z_{i}}\left(\alpha_{i}(t)-\theta_{i}(t)\right)$ and $m_{i}>0$ is the moment of inertia

## Linearized power flow balance at each bus $i$

$$
0=P_{i}(t)+P_{e, i}(t)-\sum_{j=1}^{n_{g}+n_{b}} \ell_{i j}\left(\theta_{i}(t)-\theta_{j}(t)\right)
$$

where $\ell_{i j}=\ell_{j i} \geq 0$ is the line susceptance and $P_{e, i}(t)=0$ for $i>n_{g}$

## Linear DAE model

Overall we get a linear DAE

$$
E \dot{x}=A x+B u
$$

where in our example

$$
\begin{aligned}
& x=\left(\alpha_{1}, \alpha_{2}, \omega_{1}, \omega_{2}, \theta_{1}, \theta_{2}, \theta_{3}, \theta_{4}\right)^{\top} \\
& u=\left(P_{g, 1}, P_{g, 2}, P_{1}, P_{2}, P_{3}, P_{4}\right)^{\top}
\end{aligned}
$$


and, with $\ell_{i i}:=\sum_{j=1}^{4} \ell_{i j}$,

$$
\boldsymbol{E}=\left[\begin{array}{cccccccc}
1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\
0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\
0 & 0 & m_{1} & 0 & 0 & 0 & 0 & 0
\end{array}\right)
$$

## General DAE-structure

DAE-model for $n_{g}$ generators and $n_{b}$ busses has the following structure:

$$
E \dot{x}=A x+B u
$$

(powerDAE)
with

$$
\begin{aligned}
& x=\left(\alpha_{1}, \ldots, \alpha_{n_{g}}, \omega_{1}, \ldots, \omega_{n_{g}}, \theta_{1}, \theta_{2}, \ldots, \theta_{n_{g}+n_{b}}\right)^{\top} \\
& u=\left(P_{g, 1}, \ldots, P_{g, n_{g}}, P_{1}, \ldots, P_{n_{g}+n_{b}}\right)^{\top}
\end{aligned}
$$

and

$$
\left.E=\left[\begin{array}{ccc}
I_{n_{g}} & 0 & 0 \\
0 & M & 0 \\
0 & 0 & 0
\end{array}\right], \quad A=\left[\begin{array}{ccc}
0 & I_{n_{g}} & 0 \\
-Z^{-1} & -D & {\left[\begin{array}{cc}
z^{-1} & 0
\end{array}\right]} \\
{\left[z^{-1}\right.} \\
0
\end{array}\right] \begin{array}{cc}
0 & -\mathfrak{L}-\left[\begin{array}{cl}
z_{0}^{-1} & 0 \\
0 & 0
\end{array}\right]
\end{array}\right], \quad B=\left[\begin{array}{cc}
0 & 0 \\
I_{n_{g}} & 0 \\
0 & I_{n_{g}+n_{b}}
\end{array}\right]
$$

where $\mathfrak{L}=\left[\ell_{i j}\right]$ is the (weighted) Laplacian matrix of the network groningen

## Solvability and Stability

## Theorem (Solvability and Stability, Groß et al. 2016)

Consider a power grid network and assume that is connected. Then > (powerDAE) is regular, i.e. existence and uniqueness of solutions
> (powerDAE) has index one, i.e. it is numerically well posed
> (powerDAE) is stable, i.e. all solutions remain bounded
T.B. Gross, S. Trenn, A. Wirsen: Solvability and stability of a power system DAE model, Syst. Control Lett., 29, pp. 12-17, 2016.

## Remark

Result remains true for multiple-rotating mass models of generators.


## Topological changes



$$
\begin{array}{ll}
E_{1} \dot{x}=A_{1} x+B_{1} u & \text { in mode } 1 \\
E_{2} \dot{x}=A_{2} x+B_{2} u & \text { in mode } 2
\end{array}
$$

or, introducing a switching signal $\sigma: \mathbb{R} \rightarrow\{1,2\}$

$$
E_{\sigma(t)} \dot{X}=A_{\sigma(t)} x+B_{\sigma(t)} u
$$

In fact, topological changes (removal / addition / parameter changes of lines) only effect Laplacian matrix $\mathfrak{L}$ !
$E=\left[\begin{array}{ccc}I_{n_{g}} & 0 & 0 \\ 0 & M & 0 \\ 0 & 0 & 0\end{array}\right], \quad A_{\sigma(t)}=\left[\begin{array}{ccc}0 & I_{n_{g}} & 0 \\ -Z^{-1} & -D & {\left[\begin{array}{c}z^{-1} \\ 0\end{array}\right]} \\ {\left[z^{-1}\right]} & 0 & -\mathfrak{L}_{\sigma(t)}-\left[\begin{array}{cc}z^{-1} & 0 \\ 0 & 0\end{array}\right]\end{array}\right], \quad B=\left[\begin{array}{cc}0 & 0 \\ I_{n_{g}} & 0 \\ 0 & I_{n_{g}+n_{b}}\end{array}\right]$

## Simulation



Parameters:
$m_{1}=m_{2}=1$
$z_{1}=z_{2}=0.1$
$D_{1}=D_{2}$
and La

$$
\mathfrak{L}_{1}=\left[\begin{array}{cccc}
0.01 & 0 & 0.005 & 0.005 \\
\hdashline 0 & -5.005 & 0.005 & 5 \\
0.005 & 0.005 & -0.02 & 0.01 \\
0.005 & 5 & 0.01 & -5.015
\end{array}\right], \quad \mathfrak{L}_{2}=\left[\begin{array}{cccc} 
& 0.005 & 2 \\
0.005 & 0 & 0.005 & 0.005 \\
0.005 & 0.005 & -0.02 & 0.01 \\
2 & 5 & 0.01 & -7.01
\end{array}\right]
$$

## Modelling

## Instability due to switching

## Sufficient condition for stability under arbitrary switching

## Stability and Lyapunov functions

$$
E_{\sigma} \dot{X}=A_{\sigma} X
$$

(swDAE)

## Theorem (cf. Liberzon and T. 2012)

Assume (swDAE) to be regular and index one. If

1. each mode is stable with Lyapunov function $V_{p}(\cdot)$
2. $V_{q}\left(\Pi_{q} x\right) \leq V_{p}(x)$ for all $p, q$ and all $x \in \operatorname{im} \Pi_{p}$ then (swDAE) is stable under arbitrary switching.
D. Liberzon, S. Trenn: Switched nonlinear differential algebraic equations: Solution theory, Lyapunov functions, and stability. Automatica, 48 (5), pp. 954-963, 2012.

## Remark

If $E$-matrix is switch-independent and has the form $E=\left[\begin{array}{cc}E_{1} & 0 \\ 0 & 0\end{array}\right]$ with invertible $E_{1}$, then $V_{q}\left(\Pi_{q} x\right)=V_{q}(x)$ for all $x \in \operatorname{im} \Pi_{p}$.
$\hookrightarrow$ common Lyapunov function guarantees stability

## Key lemma

## Lemma

Consider ( $E, A$ ) with structure

$$
E=\left[\begin{array}{ccc}
E_{1} & 0 & 0 \\
0 & 0 & 0 \\
0 & 0 & 0
\end{array}\right], \quad A=\left[\begin{array}{ccc}
A_{1} & A_{2} & 0 \\
A_{3} & -\mathfrak{L}_{1}+A_{4} & -\mathfrak{L}_{2} \\
0 & -\mathfrak{L}_{3} & -\mathfrak{L}_{4}
\end{array}\right],
$$

where $\mathfrak{L}=\left[\begin{array}{ll}\mathfrak{L}_{1} & \mathfrak{L}_{2} \\ \mathfrak{L}_{3} & \mathfrak{L}_{4}\end{array}\right]$ is a (weighted) Laplacian matrix. If
> $(E, A)$ is regular, index one and stable
> $\operatorname{rank} \mathfrak{L}_{3}=1$
then $\exists$ common Lyapunov function for all possible $\mathfrak{L}_{4}$

## Structural assumption for stability

Assume $\mathfrak{V}=\mathfrak{V}_{g}$ U் $\mathfrak{V}_{c}$ ப் $\mathfrak{V}_{l}$ such that

1. $\mathfrak{V}_{g}$ are the generator busses
2. no edges between $\mathfrak{V}_{g}$ and $\mathfrak{V}_{l}$
3. full connection between $\mathfrak{V}_{g}$ and $\mathfrak{V}_{c}$
4. Laplacian of edges between $\mathfrak{V}_{g}$ and $\mathfrak{V}_{c}$ has rank one
5. topological changes only occur in
 edges in $\mathfrak{N}_{c} \cup \mathfrak{V}_{l}$

## Theorem (Groß et al. 2018)

Under above assumptions, stability is preserved under arbitrary switching.
T.B. Gross, S. Trenn, A. Wirsen: Switch induced instabilities for stable power system DAE models. To appear in Proceedings of IFAC Conference on Analysis and Design of Hybrid Systems (ADHS 2018), Oxford, UK, 2018.

## Summary

> Presented a simple linear DAE-model for power grids
, This DAE model is regular, index 1 and stable
> Sudden repeated changes in line parameter may lead to instability
> Topological conditions are presented which prevent instability

## Open questions

> Physical interpretation
> Nonlinear and more detailed model

